SEKOLAH KEJURUTERAAN MEKANIKAL UNIVERSITI TEKNOLOGI MALAYSIA

SKMM 2413 THERMODYNAMICS TEST 2

QUESTION 1

a) An ideal gas undertaken an expansion process according PV = constant law. Prove that the boundary work, W_{12} , for such process is given by

$$W_{12} = P_l V_l \ln \frac{V_2}{V_l}$$

where P = pressure (kPa) and V = volume (m³)

- b) Air initially at 800 kPa, 600 K and 0.25 m³ contain in a piston-cylinder assembly undergoes a thermodynamics cycle as follows
 - 1-2: expansion process according to polytropic law, PV^n = constant, (where n = 1) until the volume increased to 0.5 m³;
 - 2-3: isobaric compression until initial volume is achieved; and
 - 3-1: isochoric(isometric) process to initial pressure.
 - i) Determine the pressure (kPa), temperature (K) and volume (m³) for state 2 and 3.
 - ii) Sketch the cycle on a P V diagram and label all the pressure, temperature and volume.
 - iii)Calculate the boundary work (kJ) for each process.
 - iv)Evaluate the heat transfer (kJ) involved for each process.
 - v) Determine the change of internal energy (kJ) for each process.
 - vi)Show that the change of internal energy (kJ) for the entire cycle is positive, negative or zero.

Table	Q1:	Pro	perties	of	air
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Property	R	Ср	Cv	k
	(kJ/kg.K)	(kJ/kg.K)	(kJ/kg.K)	
Value	0.2870	1.005	0.718	1.4000

(20 marks)

QUESTION 2

a) Steam flows steadily into a well-insulated turbine with a mass flow rate of 6 kg/s and a negligible velocity at 600 kPa and 550°C. The steam leaves the turbine through a 1.12 m diameter opening at 10 kPa with a velocity of 18 m/s. If the changes of kinetic and potential energies were neglected, determine the power output produced (*MW*).

(16 marks)

 b) If the turbine was not insulated, what would be the effect on the power output? Discuss briefly.

(4 marks)

QUESTION 3

a) i) State the four processes that make up the Carnot cycle?
ii) 'It might be possible to develop an updated heat-engine that could be more efficient than a Carnot heat engine operating between the same temperature limits.' Is the statement true or false? Why?

(4 marks)

b) An inventor claims to have developed a refrigeration system that removes heat from the closed region at -12°C and transfers it to the surrounding air at 25°C while maintaining a COP of 7.0. Is this claim reasonable or not? Justify your answer with calculation.

(6 marks)

- c) A steam power plant receives heat from a furnace at a rate of 280 GJ/h. Heat losses to the surrounding air from the steam as it passes through the pipes and other components are estimated to be about 8 GJ/h. If the waste heat is transferred to the cooling water at a rate of 145 GJ/h, determine
 - (i) the net power output (MW), and
 - (ii) the thermal efficiency of this power plant (%).

(12 marks)

TABLE A-5												
Saturat	Saturated water—Pressure table											
		<i>Specif</i>	<i>fic volume,</i> n ³ /kg	Internal energy, kJ/kg		Enthalpy, kJ/kg			<i>Entropy,</i> kJ/kg · К			
Press., <i>P</i> kPa	Sat. temp., <i>T</i> _{sat} °C	Sat . Iiquid, v _f	Sat. vapor, v _g	Sat. Iiquid, <i>u_f</i>	Evap., u _{fg}	Sat . vapor, <i>u_g</i>	Sat. Iiquid, <i>h_f</i>	Evap., h _{fg}	Sat. vapor, <i>h_g</i>	Sat. Iiquid, <i>s_f</i>	Evap., s _{fg}	Sat. vapor, <i>s_g</i>
4.0 5.0 7.5 10 15	28.96 32.87 40.29 45.81 53.97	0.001004 0.001005 0.001008 0.001010 0.001014	34.791 28.185 19.233 14.670 10.020	121.39 137.75 168.74 191.79 225.93	2293.1 2282.1 2261.1 2245.4 2222.1	2414.5 2419.8 2429.8 2437.2 2448.0	121.39 137.75 168.75 191.81 225.94	2432.3 2423.0 2405.3 2392.1 2372.3	2553.7 2560.7 2574.0 2583.9 2598.3	0.4224 0.4762 0.5763 0.6492 0.7549	8.0510 7.9176 7.6738 7.4996 7.2522	8.4734 8.3938 8.2501 8.1488 8.0071
450 500 550 600 650	147.90 151.83 155.46 158.83 161.98	0.001088 0.001093 0.001097 0.001101 0.001104	0.41392 0.37483 0.34261 0.31560 0.29260	622.65 639.54 655.16 669.72 683.37	1934.5 1921.2 1908.8 1897.1 1886.1	2557.1 2560.7 2563.9 2566.8 2569.4	623.14 640.09 655.77 670.38 684.08	2120.3 2108.0 2096.6 2085.8 2075.5	2743.4 2748.1 2752.4 2756.2 2759.6	1.8205 1.8604 1.8970 1.9308 1.9623	5.0356 4.9603 4.8916 4.8285 4.7699	6.8561 6.8207 6.7886 6.7593 6.7322

ATTACHMENT

TABLE A-6

Superheated water												
T	v	u	h	s	v	u	h	s	v	u	h	s
°C	m ³ /kg	kJ/kg	kJ/kg	kJ/kg⋅K	m ³ /kg	kJ/kg	kJ/kg	kJ/kg · K	m ³ /kg	kJ/kg	kJ/kg	kJ/kg · K

					1						
	P = 0.50 MPa (151.83°C)			P = 0.60 MPa (158.83°C)				P = 0.80 MPa (170.41°C)			
Sat.	0.37483	2560.7	2748.1	6.8207	0.31560	2566.8	2756.2	6.7593	0.24035 2576.0	2768.3	6.6616
200	0.42503	2643.3	2855.8	7.0610	0.35212	2639.4	2850.6	6.9683	0.26088 2631.1	2839.8	6.8177
250	0.47443	2723.8	2961.0	7.2725	0.39390	2721.2	2957.6	7.1833	0.29321 2715.9	2950.4	7.0402
300	0.52261	2803.3	3064.6	7.4614	0.43442	2801.4	3062.0	7.3740	0.32416 2797.5	3056.9	7.2345
350	0.57015	2883.0	3168.1	7.6346	0.47428	2881.6	3166.1	7.5481	0.35442 2878.6	3162.2	7.4107
400	0.61731	2963.7	3272.4	7.7956	0.51374	2962.5	3270.8	7.7097	0.38429 2960.2	3267.7	7.5735
500	0.71095	3129.0	3484.5	8.0893	0.59200	3128.2	3483.4	8.0041	0.44332 3126.6	3481.3	7.8692
600	0.80409	3300.4	3702.5	8.3544	0.66976	3299.8	3701.7	8.2695	0.50186 3298.7	3700.1	8.1354
700	0.89696	3478.6	3927.0	8.5978	0.74725	3478.1	3926.4	8.5132	0.56011 3477.2	3925.3	8.3794
800	0.98966	3663.6	4158.4	8.8240	0.82457	3663.2	4157.9	8.7395	0.61820 3662.5	4157.0	8.6061
900	1.08227	3855.4	4396.6	9.0362	0.90179	3855.1	4396.2	8.9518	0.67619 3854.5	4395.5	8.8185
1000	1.17480	4054.0	4641.4	9.2364	0.97893	4053.8	4641.1	9.1521	0.73411 4053.3	4640.5	9.0189
1100	1.26728	4259.0	4892.6	9.4263	1.05603	4258.8	4892.4	9.3420	0 79197 4258 3	4891.9	9.2090
1200	1.35972	4470.0	5149.8	9.6071	1.13309	4469.8	5149.6	9.5229	0.84980 4469.4	5149.3	9.3898
1300	1.45214	4686.6	5412.6	9.7797	1.21012	4686.4	5412.5	9.6955	0.90761 4686.1	5412.2	9.5625



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· 0)	PV=C, P=C/V	$W_{23} = P_2(V_3 - V_2)$	- Y2
	$W_{12} = \int p dV = C \int dV - 2$	= 400 (0.25-0.5)	
		= -100.00 kJ	- 12
	$= C \ln V = P_1 V_1 (\ln V_2 - \ln V_1)$	W ₃₁ = 0	-1 12
	= P,V, In V2/V, *	iv) Q12·mCv (Iz=Fr)+W12	- 1/2/
	[4]	Q1= W1= 138.63 +J -	- 1/2,
b)	PI= 800 KPA expansion 12=0.5m3		
	$T_1 = 600 \text{ K}$ $T_2 = T_1$	$Q_{23} = m C_v (T_3 - T_2) + W_{23}$	- 1/2
	V = 0.25m ² T=C	$m = P_1 V_1 = 800 \times 0.25 = 1.161$	4 kg - 1
	Heating Compression	1, 0.287 × 600	•
	Y= c P= C	Q23 = 1.1614×0.718 (300-600)+	(-100.00)
		=-350.17 kJ	1/2
	P3=P2	OR Q23=m (p (T3-T2)	1
	i) $P_2 = P_1 V_1 = 800 \times 0.25$	\$23 = X1614 × 1.005 × 300-600)=-	350.16kJ
0	V ₂ 0.5	Q31=m(v(T,-T3)+W370 -	
12= A00 + B	-> Pa = 400 kPa ; 1/2	= 1.1614 × 0.718 (600-300)	
T2: 600Klg	$\rightarrow T_2: T_1: 600 \text{K} - \text{K}$	= 250.17 kJ	Y2 4
$V_2 = 0.5m^2$	$\rightarrow V_2 = 0.5 \text{ m}^3 - \frac{1}{2}$	_0	
P3 = 400 kg	$P_2 = P_2 = AOO \times Pq - h$	V) 6Up = m(v(It) = 0 -	1
$T_3 = 300 \text{ K}$	R3 Y3 = R2 V2 T3 = T2 V3	AU23 = Q23 - W23	-12
V2=0.25m3	T3 T2 V2	= -350.17 - (-100.00)	
	$T_3 = 600 \times 0.25 = 300 \text{ K} - \text{K}$	= -250.17 kJ	-n ₁
	0.5	QU31 = Q31 - 4310	_ n
	$Y_3 = V_1 = 0.25 m^3 - h$	= 250,17kJ	- Ky 3
•	3		
	ii) R + X R = C	$vi) Z \Delta U = \Delta U_{12} + \Delta U_{23} + \Delta U_{23}$	31
	V=C V B	= 0 + (-250.17) + 250.13	
		= 0	<u> </u>
	$P_2 = P_3 = \frac{1}{3} + \frac{1}{3} + \frac{1}{10} = C_1 = T_1 = T_2$	$OR ZQ = Q_{12} + Q_{23} + Q_{31}$	
		= 138.63+(350.17)+2	5017
		= 38.63KJ	
	111) W12= PiVi In V2/V 12	$ZW = W_{12} + W_{23} + W_{31}$	
	= 800×0.25 m 0.5	= 138.63+(-100.00) +	0
	= 138.63 kJ - 0.25 1/2	= 38.63 KJ > ZQ=	ΞW



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	2	h=hp +	zhee	3	
Valle	,	f 17	1(12	
ŤΤ		$\chi_n = V_n$	-Vfr		
1	/	Ver	- Ver		
""		: 2.95	556-0.	001010	
m= Gkg/s	$d_2 = 1.12 m$	14.6	70 - 0.	001010	
$P_1 = 600 \text{ kg}$	P2=10×Pa	= 0.2	014	••••••••••••••••••••••••••••••••••••••	_ 2
T1 = 550°C	$\nabla_2 = 18 m/s$	h = 191.81-	+ 0.2014	+ (2392.1)	
SKE-0 D	PE = 0	= 673.6	KS/Kg	j	<u> </u>
Win = m Wiz		W12 = 3592.	6 - 673	.6	
$h_1 = h_2 + U$	Niz	= 2919	· OKJ/	5	
$W_{12} = h_1 - 1$	n, <u>Z</u>	$W_{12} = 6 \times 7$	2919.0	0	
State 1: At a	500kpa Tsat = 158-830	= 1751	4 KW		
Ti>Trat	s.h.v	٩	17.5	ww -	
At 0.6Mpa					-
h T		b) Wiz will	decrea	sed!	
3483.4 500		W12 = (h1-	$(h_2) -$	Qloss	· · · · · · · · · · · · · · · · · · ·
h, 550	<u> </u>	Win' L Wi-	2		<u> </u>
3701.7 600					
h 3483.4	= 50	•			
3701.7-3483.1	+ 100	(a) + ((b)		
h = 3592.6	KJ/Kg	16 +	4 =	20	
	0	16	4	20	
State 2: P2	= 101299				
$\dot{m} = A_1 V_1$	Va= AnVa		General 1		and and the second s
Va,	Ŵ				
An = Tidz = -	TI X 1.122				
Ā	4				
= 0.9852	m ³ — 1	350011			
V= 0.9852	× 18				
6			······································		
= 2.9556	$m^{3}/k_{9} - 3$			······	
At IOKPA V	ILV2LVa				
. sat. mi	xt22				
					L



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	Q3 No. Soalan Question No.	Muka surat Page	apa di ruangan ini Do not write anything in this column
a);	1-2: Revensible is thermal exp.	ii) 7. = Whet. ont	-
	2-3: Reversible adia batic exp. 2	th Qu	
	3-4: Reversible isothermal comp.	<u> </u>	
	4-1: Reversible adrabatic comp.	= 35.28×10 ×10	0
ii)	False! 7th > 7th all -1	1280 ×106)	
		3600	
b)	TH= 298K	= 45.36%	- 4
,	Q_{H} $COP_{R} = 7.0$		
	(R) K- When, M		
	Ja-	(a) + (b)	
	TL=261K	4 + 16 = 20	
	Cop = =	4 16 20	
	= = 7.05		·
	298 - 1		
	261 -5		
	COP L COP		
	. a wevernble cycle!		
	The claim is reasonable.		
``			-
c)			
	$\varphi Q_{\mu} = 280 \text{GJ/h}$		
	(HE) -> Whet, out		- -
	V @_= 01145=15505		
	1) What and $= (0, -0)$		
	= 280-153		
	= 127 (GJ × h)		
	h 36005)	· · · · · · · · · · · · · · · · · · ·	
	= 0.03528/dw x10M)		
	= 35.28 MW $- 4,$		
	/ 1	· · · · · · · · · · · · · · · · · · ·	