

HEAT TRANSFER

SETN2223



UTM
UNIVERSITI TEKNOLOGI MALAYSIA

RADIATION EXCHANGE BETWEEN SURFACES

www.utm.my

innovative • entrepreneurial • global



univteknologimalaysia



utm_my



utmofficial

THE VIEW FACTOR

13.1.1 The View Factor Integral

The view factor F_{ij} is defined as the *fraction of the radiation leaving surface i that is intercepted by surface j* . To develop a general expression for F_{ij} , we consider the arbitrarily oriented surfaces A_i and A_j of Figure 13.1. Elemental areas on each surface, dA_i and dA_j , are connected by a line of length R , which forms the polar angles θ_i and θ_j , respectively, with the surface normals \mathbf{n}_i and \mathbf{n}_j . The values of R , θ_i , and θ_j vary with the position of the elemental areas on A_i and A_j .

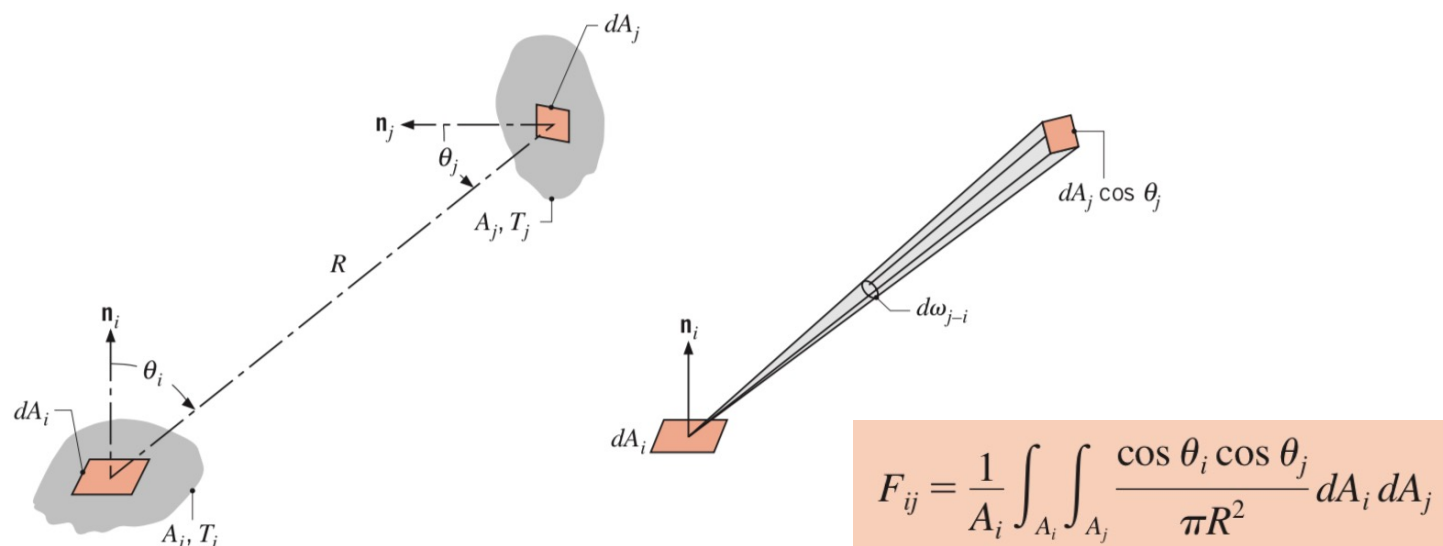


FIGURE 13.1 View factor associated with radiation exchange between elemental surfaces of area dA_i and dA_j .

THE VIEW FACTOR

13.1.2 View Factor Relations

An important view factor relation is suggested by Equations 13.1 and 13.2. In particular, equating the integrals appearing in these equations, it follows that

$$A_i F_{ij} = A_j F_{ji} \quad (13.3)$$

This expression, termed the *reciprocity relation*, is useful in determining one view factor from knowledge of the other.

$$F_{21} = \left(\frac{A_1}{A_2} \right) F_{12} = \left(\frac{A_1}{A_2} \right)$$

THE VIEW FACTOR

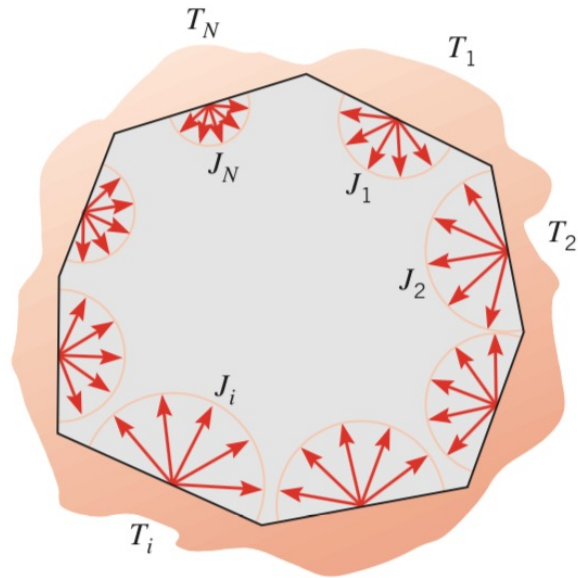


FIGURE 13.2 Radiation exchange in an enclosure.

Another important view factor relation pertains to the surfaces of an *enclosure* (Figure 13.2). From the definition of the view factor, the *summation rule*

$$\sum_{j=1}^N F_{ij} = 1 \quad (13.4)$$

THE VIEW FACTOR

$$\sum_{j=1}^N F_{ij} = 1 \quad (13.4)$$

may be applied to each of the N surfaces in the enclosure. This rule follows from the conservation requirement that all radiation leaving surface i must be intercepted by the enclosure surfaces. The term F_{ii} appearing in this summation represents the fraction of the radiation that leaves surface i and is directly intercepted by i . If the surface is concave, it *sees itself* and F_{ii} is nonzero. However, for a plane or convex surface, $F_{ii} = 0$.

To calculate radiation exchange in an enclosure of N surfaces, a total of N^2 view factors is needed. This requirement becomes evident when the view factors are arranged in the matrix form:

$$\begin{bmatrix} F_{11} & F_{12} & \cdots & F_{1N} \\ F_{21} & F_{22} & \cdots & F_{2N} \\ \vdots & \vdots & & \vdots \\ F_{N1} & F_{N2} & \cdots & F_{NN} \end{bmatrix}$$

THE VIEW FACTOR

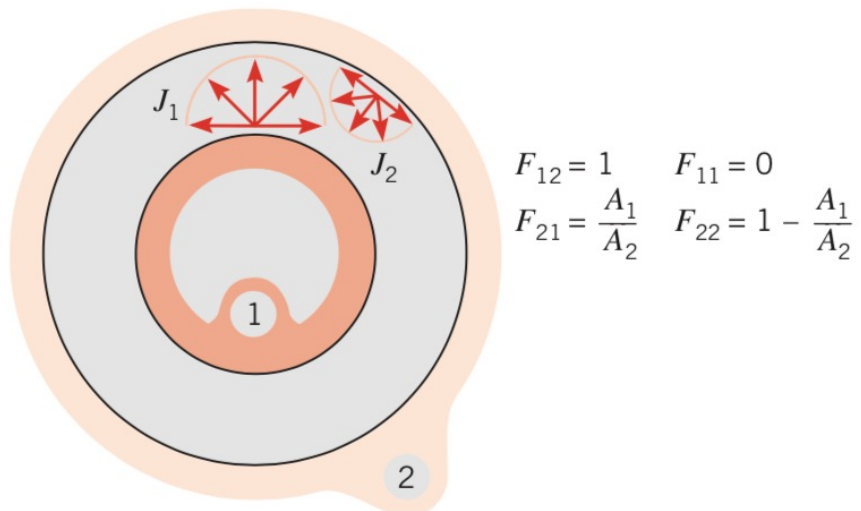


FIGURE 13.3 View factors for the enclosure formed by two spheres.

From the summation rule, we also obtain

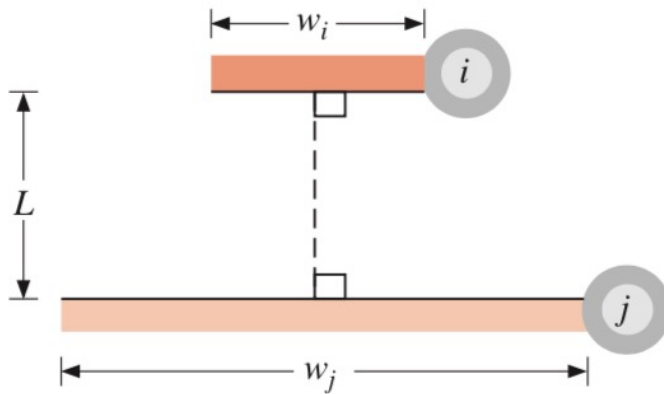
$$F_{11} + F_{12} = 1$$

in which case $F_{11} = 0$, and

$$F_{21} + F_{22} = 1$$

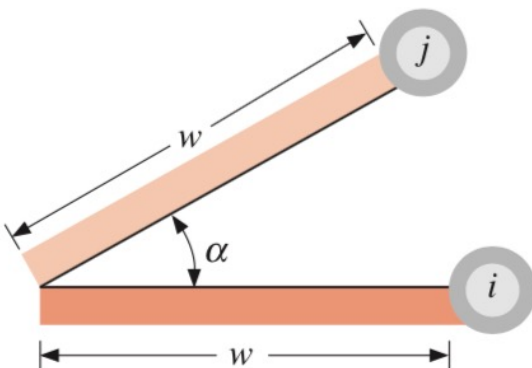
in which case

$$F_{22} = 1 - \left(\frac{A_1}{A_2} \right)$$

TABLE 13.1 View Factors for Two-Dimensional Geometries [4]**Geometry****Relation****Parallel Plates with Midlines
Connected by Perpendicular**

$$F_{ij} = \frac{[(W_i + W_j)^2 + 4]^{1/2} - [(W_j - W_i)^2 + 4]^{1/2}}{2W_i}$$

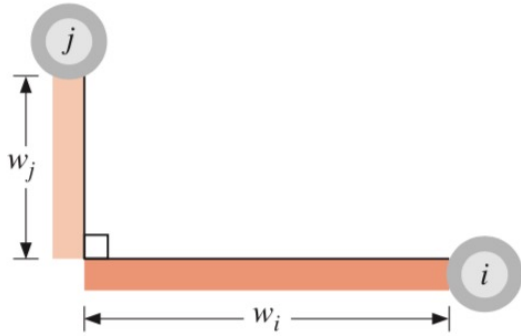
$$W_i = w_i/L, W_j = w_j/L$$

**Inclined Parallel Plates of Equal
Width and a Common Edge**

$$F_{ij} = 1 - \sin\left(\frac{\alpha}{2}\right)$$

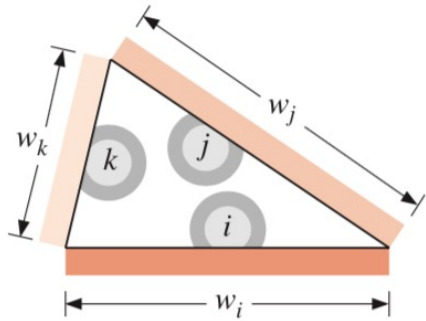
(continues)

Perpendicular Plates with a Common Edge



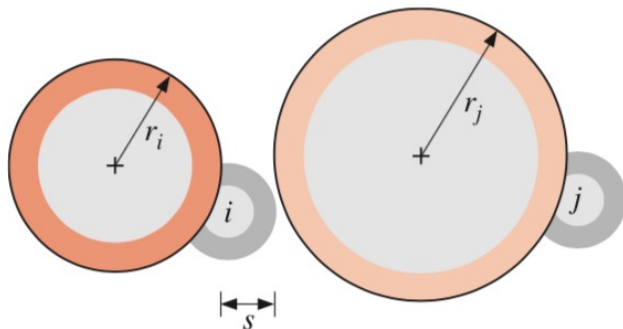
$$F_{ij} = \frac{1 + (w_j/w_i) - [1 + (w_j/w_i)^2]^{1/2}}{2}$$

Three-Sided Enclosure



$$F_{ij} = \frac{w_i + w_j - w_k}{2w_i}$$

Parallel Cylinders of Different Radii

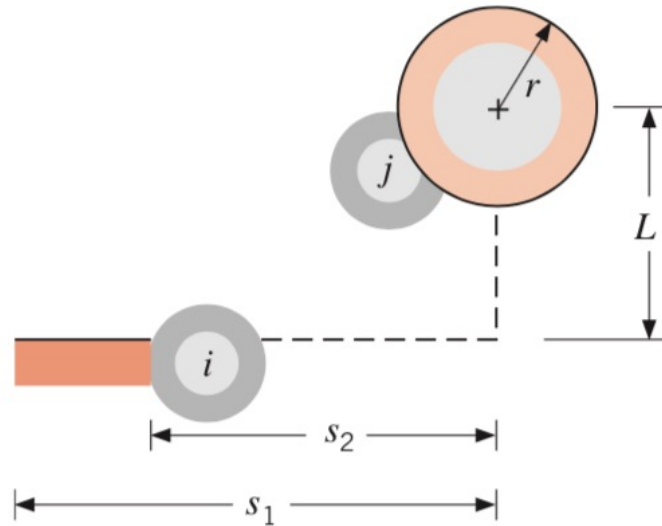


$$F_{ij} = \frac{1}{2\pi} \left\{ \pi + [C^2 - (R + 1)^2]^{1/2} - [C^2 - (R - 1)^2]^{1/2} + (R - 1) \cos^{-1} \left[\left(\frac{R}{C} \right) - \left(\frac{1}{C} \right) \right] - (R + 1) \cos^{-1} \left[\left(\frac{R}{C} \right) + \left(\frac{1}{C} \right) \right] \right\}$$

$$R = r_j/r_i, S = s/r_i$$

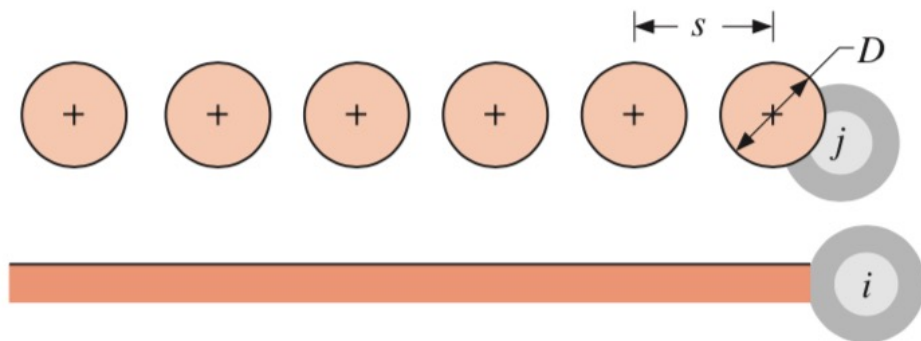
$$C = 1 + R + S$$

Cylinder and Parallel Rectangle



$$F_{ij} = \frac{r}{s_1 - s_2} \left[\tan^{-1} \frac{s_1}{L} - \tan^{-1} \frac{s_2}{L} \right]$$

Infinite Plane and Row of Cylinders



$$F_{ij} = 1 - \left[1 - \left(\frac{D}{s} \right)^2 \right]^{1/2} + \left(\frac{D}{s} \right) \tan^{-1} \left[\left(\frac{s^2 - D^2}{D^2} \right)^{1/2} \right]$$

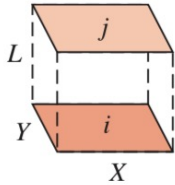
TABLE 13.2 View Factors for Three-Dimensional Geometries [4]

Geometry

Relation

Aligned Parallel Rectangles

(Figure 13.4)

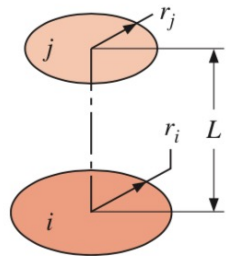


$$\bar{X} = X/L, \bar{Y} = Y/L$$

$$F_{ij} = \frac{2}{\pi \bar{X} \bar{Y}} \left\{ \ln \left[\frac{(1 + \bar{X}^2)(1 + \bar{Y}^2)}{1 + \bar{X}^2 + \bar{Y}^2} \right]^{1/2} + \bar{X}(1 + \bar{Y}^2)^{1/2} \tan^{-1} \frac{\bar{X}}{(1 + \bar{Y}^2)^{1/2}} + \bar{Y}(1 + \bar{X}^2)^{1/2} \tan^{-1} \frac{\bar{Y}}{(1 + \bar{X}^2)^{1/2}} - \bar{X} \tan^{-1} \bar{X} - \bar{Y} \tan^{-1} \bar{Y} \right\}$$

Coaxial Parallel Disks

(Figure 13.5)



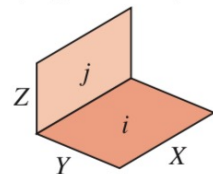
$$R_i = r_i/L, R_j = r_j/L$$

$$S = 1 + \frac{R_j^2}{R_i^2}$$

$$F_{ij} = \frac{1}{2} \{ S - [S^2 - 4(r_j/r_i)^2]^{1/2} \}$$

Perpendicular Rectangles with a Common Edge

(Figure 13.6)



$$H = Z/X, W = Y/X$$

$$F_{ij} = \frac{1}{\pi W} \left(W \tan^{-1} \frac{1}{W} + H \tan^{-1} \frac{1}{H} - (H^2 + W^2)^{1/2} \tan^{-1} \frac{1}{(H^2 + W^2)^{1/2}} + \frac{1}{4} \ln \left\{ \frac{(1 + W^2)(1 + H^2)}{1 + W^2 + H^2} \left[\frac{W^2(1 + W^2 + H^2)}{(1 + W^2)(W^2 + H^2)} \right]^{W^2} \times \left[\frac{H^2(1 + H^2 + W^2)}{(1 + H^2)(H^2 + W^2)} \right]^{H^2} \right\} \right)$$

THE VIEW FACTOR

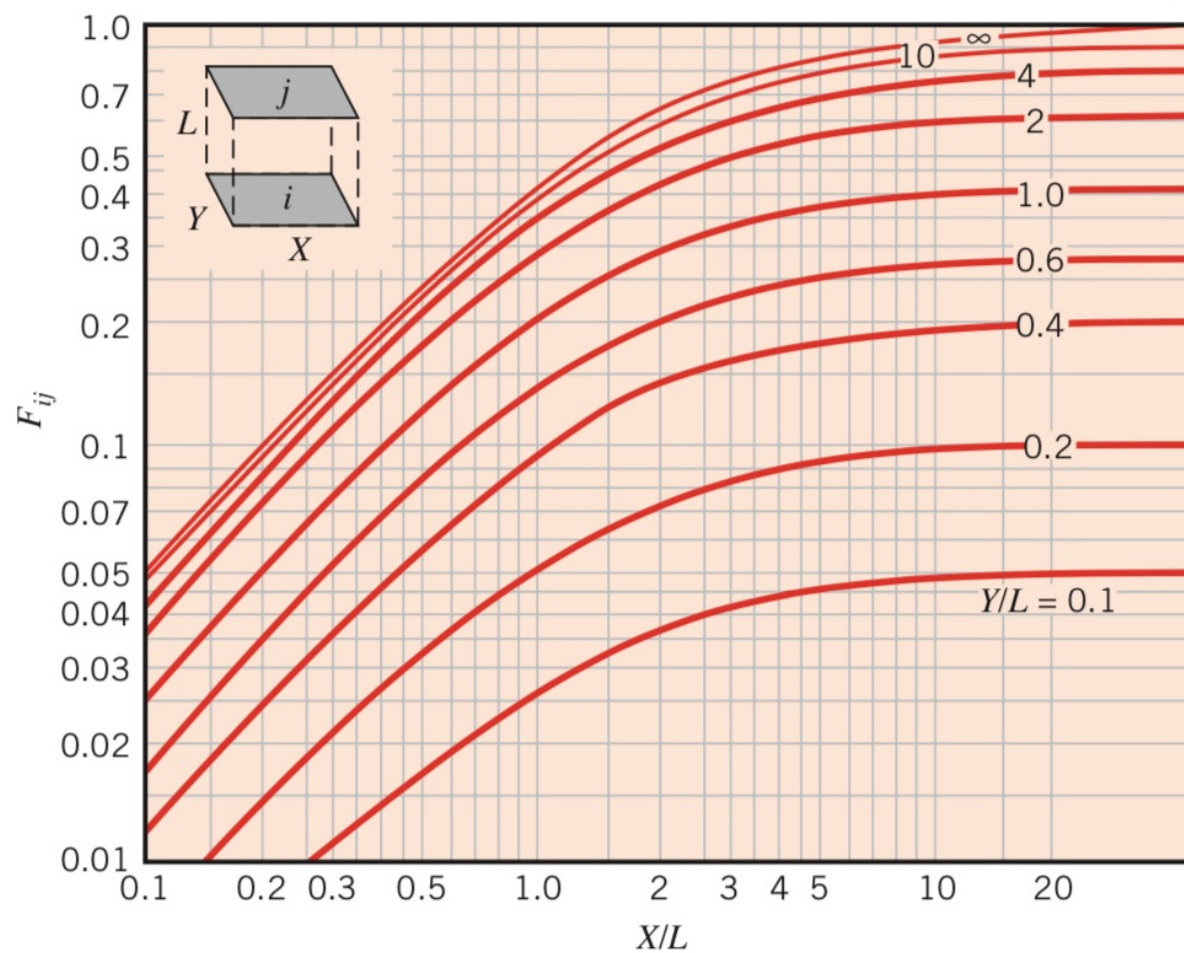


FIGURE 13.4 View factor for aligned parallel rectangles.

THE VIEW FACTOR

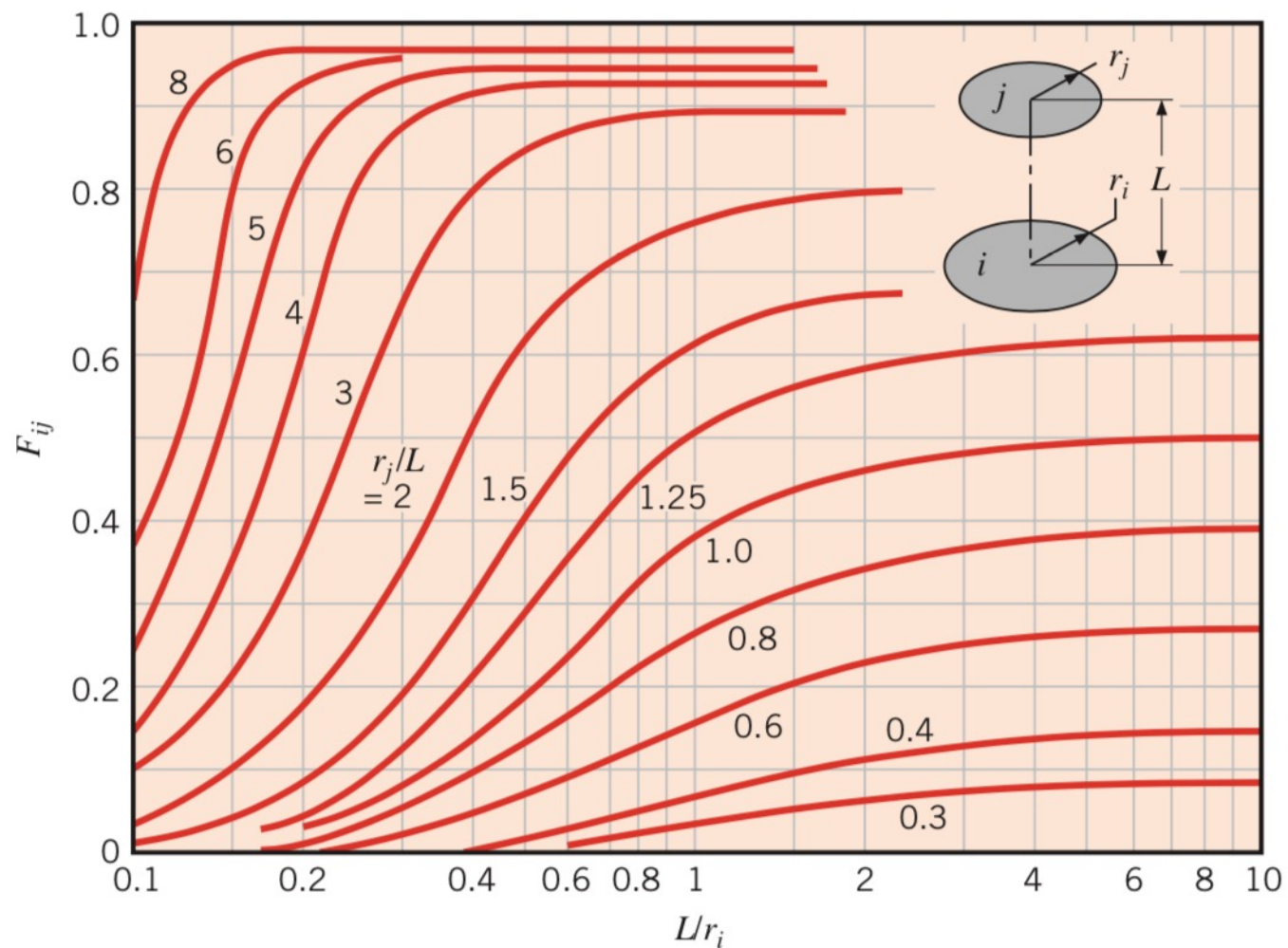


FIGURE 13.5 View factor for coaxial parallel disks.

THE VIEW FACTOR

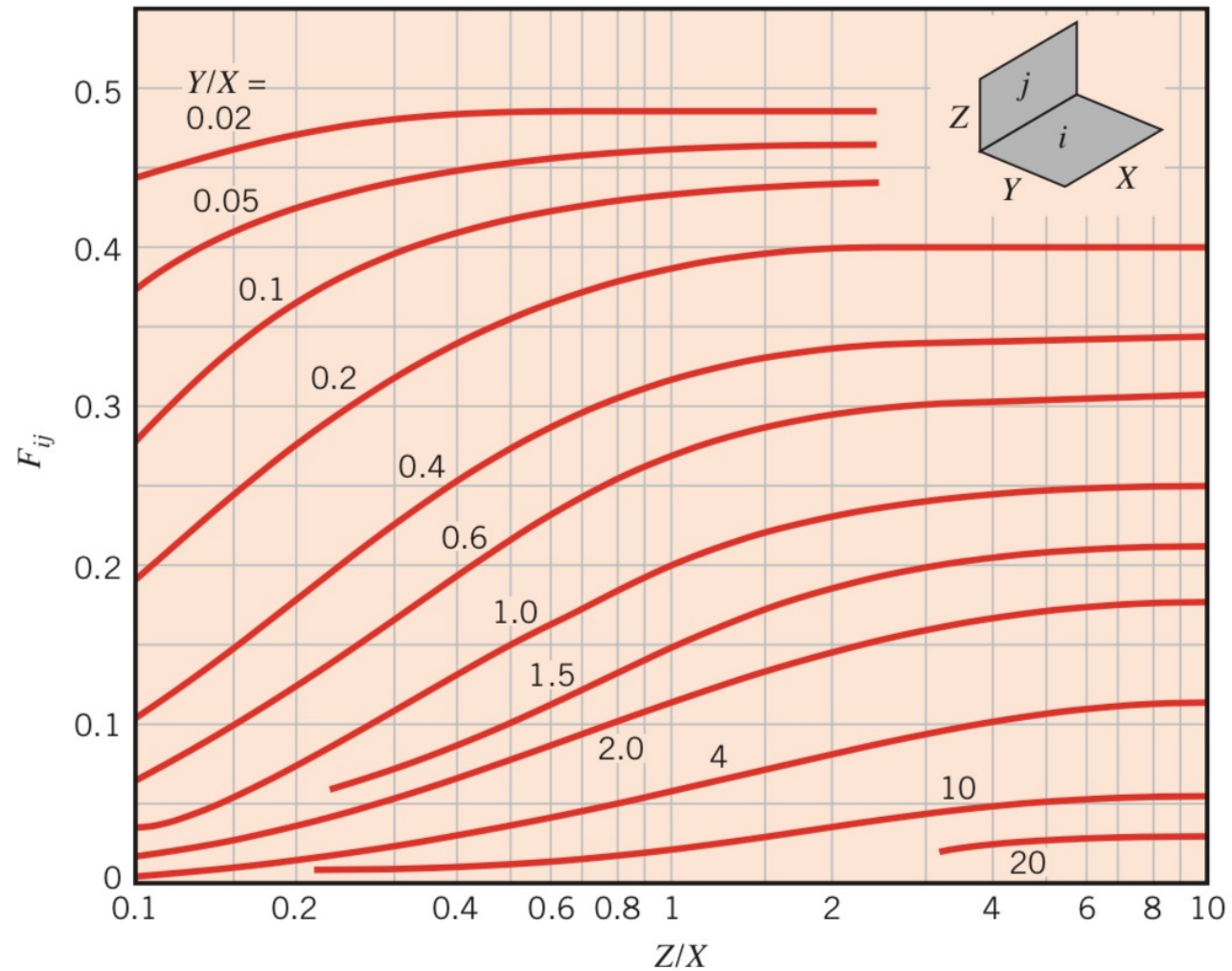


FIGURE 13.6 View factor for perpendicular rectangles with a common edge.



univteknologimalaysia



utm_my



utmofficial

Thank You

www.utm.my

innovative • entrepreneurial • global