# HEAT TRANSFER SETN2223



## RADIATION: PROCESSES AND PROPERTIES

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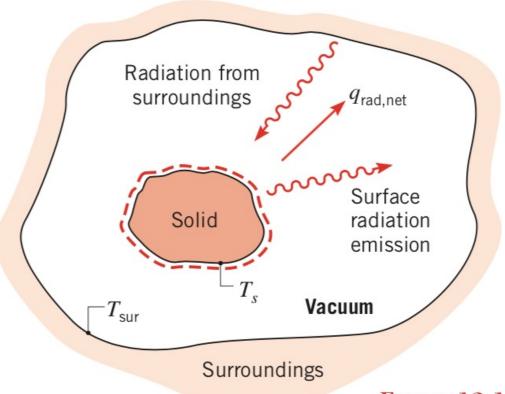


**SETN2223** 



#### **Recall**

We have come to recognize that heat transfer by **conduction** and **convection** requires the presence of a **temperature gradient** in some form of **matter** 



Thermal Radiation is electromagnetic radiation emitted by a body due to its temperature

**FIGURE 12.1** Radiation cooling of a hot solid.



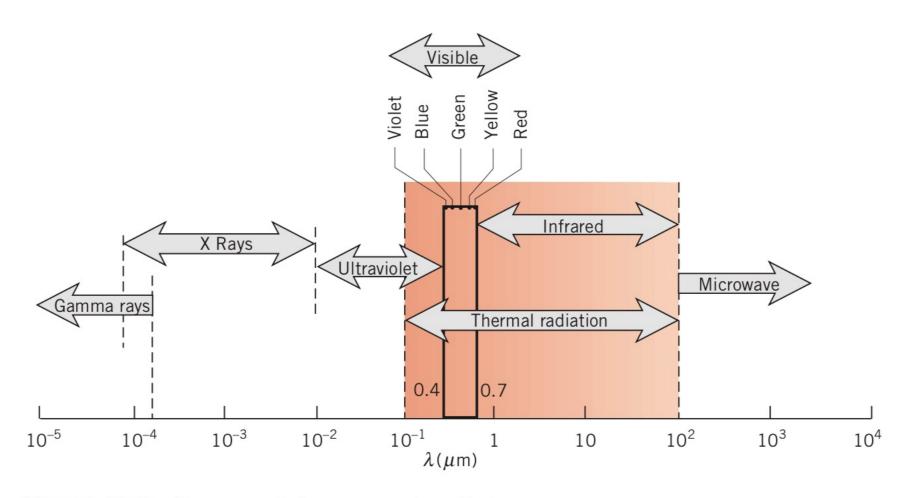
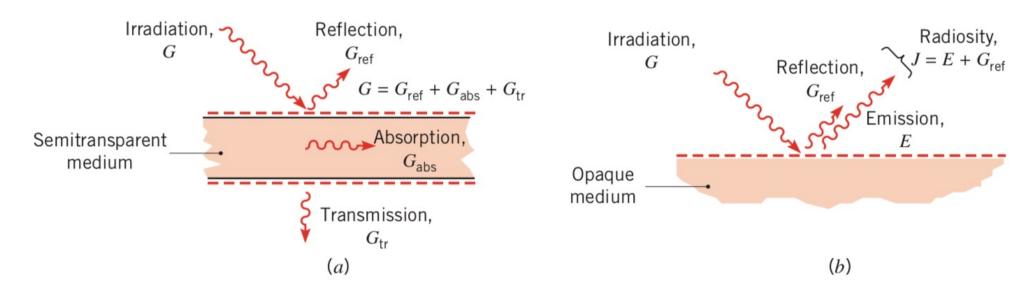


FIGURE 12.3 Spectrum of electromagnetic radiation.





**FIGURE 12.5** Radiation at a surface. (a) Reflection, absorption, and transmission of irradiation for a semitransparent medium. (b) The radiosity for an opaque medium.



Absorption occurs when radiation interacts with the medium, causing an increase in the internal thermal energy of the medium. Reflection is the process of incident radiation being redirected away from the surface, with no effect on the medium. We define reflectivity  $\rho$  as the fraction of the irradiation that is reflected, absorptivity  $\alpha$  as the fraction of the irradiation that is transmitted. Because all of the irradiation must be reflected, absorbed, or transmitted, it follows that

$$\rho + \alpha + \tau = 1 \tag{12.2}$$

A medium that experiences no transmission ( $\tau = 0$ ) is *opaque*, in which case

$$\rho + \alpha = 1 \tag{12.3}$$

With this understanding of the partitioning of the irradiation into reflected, absorbed, and transmitted components, two additional and useful radiation fluxes can be defined. The *radiosity*,  $J(W/m^2)$ , of a surface accounts for *all* the radiant energy leaving the surface. For an opaque surface, it includes emission and the reflected portion of the irradiation, as illustrated in Figure 12.5b. It is therefore expressed as

$$J = E + G_{\text{ref}} = E + \rho G \tag{12.4}$$



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Radiosity can also be defined at a surface of a semitransparent medium. In that case, the radiosity leaving the top surface of Figure 12.5a (not shown) would include radiation transmitted through the medium from below.

Finally, the *net* radiative flux *from* a surface,  $q''_{rad}$  (W/m<sup>2</sup>), is the difference between the outgoing and incoming radiation

$$q_{\rm rad}^{\prime\prime} = J - G \tag{12.5}$$

Combining Equations 12.5, 12.4, 12.3, and 1.4, the net flux for an opaque surface is

$$q_{\rm rad}^{"} = E + \rho G - G = \varepsilon \sigma T_s^4 - \alpha G \tag{12.6}$$



#### **Summary:**

**TABLE 12.1** Radiative fluxes (over all wavelengths and in all directions)

Flux (W/m²)	Description	Comment
Emissive power, E	Rate at which radiation is emitted from a surface per unit area	$E = \varepsilon \sigma T_s^4$
Irradiation, $G$	Rate at which radiation is incident upon a surface per unit area	Irradiation can be reflected, absorbed, or transmitted
Radiosity, $J$	Rate at which radiation leaves a surface per unit area	For an opaque surface $J = E + \rho G$
Net radiative flux, $q''_{\text{rad}} = J - G$	Net rate of radiation leaving a surface per unit area	For an opaque surface $q''_{\rm rad} = \varepsilon \sigma T_s^4 - \alpha G$



## **Blackbody Radiation**

- **1.** A blackbody absorbs all incident radiation, regardless of wavelength and direction.
- **2.** For a prescribed temperature and wavelength, no surface can emit more energy than a blackbody.
- **3.** Although the radiation emitted by a blackbody is a function of wavelength and temperature, it is independent of direction. That is, the blackbody is a diffuse emitter.

As the perfect absorber and emitter, the blackbody serves as a *standard* against which the radiative properties of actual surfaces may be compared.

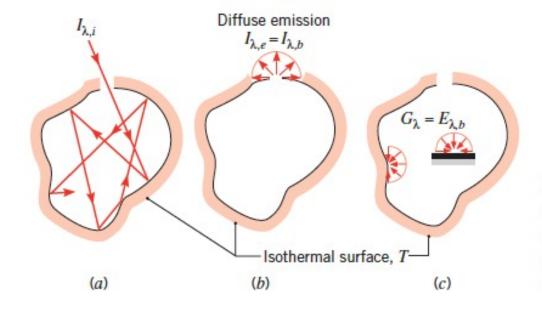


FIGURE 12.11 Characteristics of an isothermal blackbody cavity. (a) Complete absorption. (b) Diffuse emission from an aperture. (c) Diffuse irradiation of interior surfaces.



#### **Planck's Distribution**

#### **Spectral Emissive Power of a Blackbody**

$$E_{\lambda,b}(\lambda,T) = \pi I_{\lambda,b}(\lambda,T) = \frac{C_1}{\lambda^5 [\exp(C_2/\lambda T) - 1]}$$
(12.30)

where the first and second radiation constants are  $C_1 = 2\pi h c_o^2 = 3.742 \times 10^8 \text{ W} \cdot \mu \text{m}^4/\text{m}^2$  and  $C_2 = (hc_o/k_B) = 1.439 \times 10^4 \mu \text{m} \cdot \text{K}$ .

Equation 12.30, known as the *Planck distribution*, or *Planck's law*, is plotted in Figure 12.12 for selected temperatures. Several important features should be noted.

- 1. The emitted radiation varies *continuously* with wavelength.<sup>1</sup>
- **2.** At any wavelength the magnitude of the emitted radiation increases with increasing temperature.
- **3.** The spectral region in which the radiation is concentrated depends on temperature, with *comparatively* more radiation appearing at shorter wavelengths as the temperature increases.
- **4.** A significant fraction of the radiation emitted by the sun, which may be approximated as a blackbody at 5800 K, is in the visible region of the spectrum. In contrast, for  $T \lesssim 800$  K, emission is predominantly in the infrared region of the spectrum and is not visible to the eye.

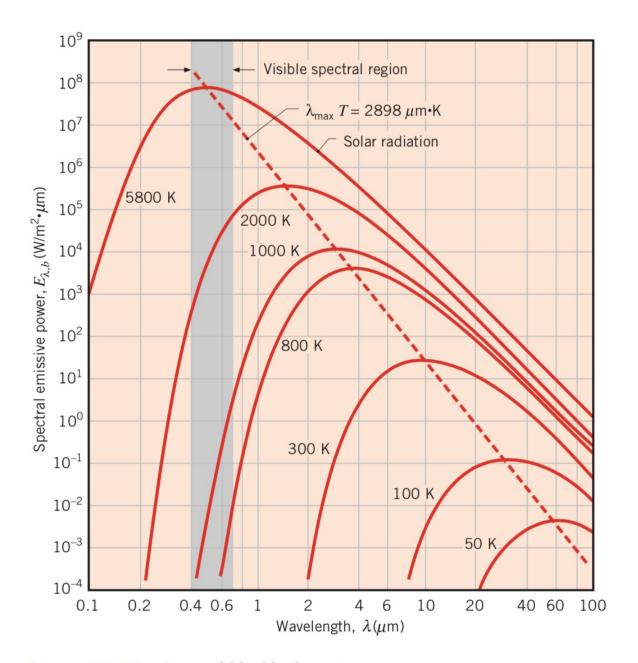


FIGURE 12.12 Spectral blackbody emissive power.





## Wien's Displacement Law

From Figure 12.12 we see that the blackbody spectral distribution has a maximum and that the corresponding wavelength  $\lambda_{max}$  depends on temperature. The nature of this dependence may be obtained by differentiating Equation 12.30 with respect to  $\lambda$  and setting the result equal to zero. In so doing, we obtain

$$\lambda_{\max} T = C_3 \tag{12.31}$$

where the third radiation constant is  $C_3 = 2898 \,\mu\text{m}\cdot\text{K}$ .

Equation 12.31 is known as *Wien's displacement law*, and the locus of points described by the law is plotted as the dashed line of Figure 12.12. According to this result, the maximum spectral emissive power is displaced to shorter wavelengths with increasing temperature. This emission is in the middle of the visible spectrum ( $\lambda \approx 0.50~\mu m$ ) for solar radiation, since the sun emits approximately as a blackbody at 5800 K. For a blackbody at 1000 K, peak emission occurs at 2.90  $\mu m$ , with some of the emitted radiation appearing visible as red light. With increasing temperature, shorter wavelengths become more prominent, until eventually significant emission occurs over the entire visible spectrum. For example, a tungsten filament lamp operating at 2900 K ( $\lambda_{max} = 1~\mu m$ ) emits white light, although most of the emission remains in the IR region.



#### Stefan-Boltzman's Law

Substituting the Planck distribution, Equation 12.30, into Equation 12.14, the total emissive power of a blackbody  $E_b$  may be expressed as

$$E_b = \int_0^\infty \frac{C_1}{\lambda^5 [\exp(C_2/\lambda T) - 1]} \, d\lambda$$

Performing the integration, it may be shown that

$$E_b = \sigma T^4 \tag{12.32}$$

where the Stefan-Boltzmann constant, which depends on  $C_1$  and  $C_2$ , has the numerical value

$$\sigma = 5.670 \times 10^{-8} \,\text{W/m}^2 \cdot \text{K}^4$$

This simple, yet important, result is termed the *Stefan–Boltzmann law*. It enables calculation of the amount of radiation emitted in all directions and over all wavelengths simply from knowledge of the temperature of the blackbody. Because this emission is diffuse, it follows



#### **Band Emission**

To account for spectral effects, it is often necessary to know the fraction of the total emission from a blackbody that is in a certain wavelength interval or *band*. For a prescribed temperature and the interval from 0 to  $\lambda$ , this fraction is determined by the ratio of the shaded section to the total area under the curve of Figure 12.13. Hence

$$F_{(0\to\lambda)} \equiv \frac{\int_0^{\lambda} E_{\lambda,b} d\lambda}{\int_0^{\infty} E_{\lambda,b} d\lambda} = \frac{\int_0^{\lambda} E_{\lambda,b} d\lambda}{\sigma T^4} = \int_0^{\lambda T} \frac{E_{\lambda,b}}{\sigma T^5} d(\lambda T) = f(\lambda T)$$
 (12.34)

Since the integrand  $(E_{\lambda,b}/\sigma T^5)$  is exclusively a function of the wavelength-temperature product  $\lambda T$ , the integral of Equation 12.34 may be evaluated to obtain  $F_{(0\to\lambda)}$  as a function of only  $\lambda T$ . The results are presented in Table 12.2 and Figure 12.14. They may also be used to obtain the fraction of the radiation between any two wavelengths  $\lambda_1$  and  $\lambda_2$ , since

$$F_{(\lambda_1 \to \lambda_2)} = \frac{\int_0^{\lambda_2} E_{\lambda,b} d\lambda - \int_0^{\lambda_1} E_{\lambda,b} d\lambda}{\sigma T^4} = F_{(0 \to \lambda_2)} - F_{(0 \to \lambda_1)}$$
(12.35)

**TABLE 12.2** Blackbody Radiation Functions

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$\lambda T$ $(\mu \mathbf{m} \cdot \mathbf{K})$	$F_{(0  ightarrow \lambda)}$	$I_{\lambda,b}(\lambda,T)/\sigma T^5$ $(\mu \mathbf{m} \cdot \mathbf{K} \cdot \mathbf{sr})^{-1}$	$\frac{I_{\lambda,b}(\lambda,T)}{I_{\lambda,b}(\lambda_{\max},T)}$
( <b>p</b> oin 11)	<b>1</b> (0 → <b>λ</b> )	(11 11 51)	7A, b (7 max) 1 )
200	0.000000	$0.375034 \times 10^{-27}$	0.000000
400	0.000000	$0.490335 \times 10^{-13}$	0.000000
600	0.000000	$0.104046 \times 10^{-8}$	0.000014
800	0.000016	$0.991126 \times 10^{-7}$	0.001372
1,000	0.000321	$0.118505 \times 10^{-5}$	0.016406
1,200	0.002134	$0.523927 \times 10^{-5}$	0.072534
1,400	0.007790	$0.134411 \times 10^{-4}$	0.186082
1,600	0.019718	0.249130	0.344904
1,800	0.039341	0.375568	0.519949
2,000	0.066728	0.493432	0.683123
2,200	0.100888	$0.589649 \times 10^{-4}$	0.816329
2,400	0.140256	0.658866	0.912155
2,600	0.183120	0.701292	0.970891
2,800	0.227897	0.720239	0.997123
2,898	0.250108	$0.722318 \times 10^{-4}$	1.000000

 TABLE 12.2
 Continued

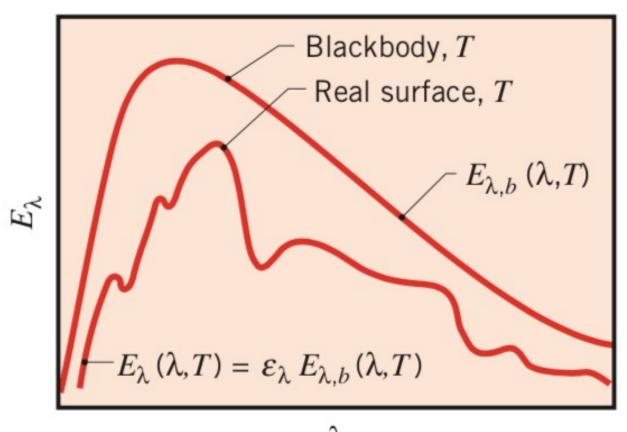
$\lambda T$		$I_{\lambda,b}(\lambda,T)/\sigma T^5$	$I_{\lambda,b}(\lambda,T)$		
$(\mu \mathbf{m} \cdot \mathbf{K})$	$F_{(0  o \lambda)}$	$(\mu \mathbf{m} \cdot \mathbf{K} \cdot \mathbf{sr})^{-1}$	$\overline{I_{\lambda,b}(\lambda_{\max},T)}$		
3,000	0.273232	$0.720254 \times 10^{-4}$	0.997143		
3,200	0.318102	0.705974	0.977373		
3,400	0.361735	0.681544	0.943551		
3,600	0.403607	0.650396	0.900429		
3,800	0.443382	$0.615225 \times 10^{-4}$	0.851737		
4,000	0.480877	0.578064	0.800291		
4,200	0.516014	0.540394	0.748139		
4,400	0.548796	0.503253	0.696720		
4,600	0.579280	0.467343	0.647004		
4,800	0.607559	0.433109	0.599610	10.500	0.923710
5,000	0.633747	0.400813	0.554898	10,500	
5,200	0.658970	$0.370580 \times 10^{-4}$	0.513043	11,000	0.931890
5,400	0.680360	0.342445	0.474092	11,500	0.939959
5,600	0.701046	0.316376	0.438002	12,000	0.945098
5,800	0.720158	0.292301	0.404671	13,000	0.955139
6,000	0.737818	0.270121	0.373965		
6,200	0.754140	$0.249723 \times 10^{-4}$	0.345724	14,000	0.962898
6,400	0.769234	0.230985	0.319783	15,000	0.969981
6,600	0.783199	0.213786	0.295973	16,000	0.973814
6,800	0.796129	0.198008	0.274128	18,000	0.980860
7,000	0.808109	0.183534	0.254090		
7,200	0.819217	$0.170256 \times 10^{-4}$	0.235708	20,000	0.985602
7,400	0.829527	0.158073	0.218842	25,000	0.992215
7,600	0.839102	0.146891	0.203360	30,000	0.995340
7,800	0.848005	0.136621	0.189143	40,000	0.997967
8,000	0.856288	0.127185	0.176079	50,000	0.998953
8,500	0.874608	$0.106772 \times 10^{-4}$	0.147819		
9,000	0.890029	$0.901463 \times 10^{-5}$	0.124801	75,000	0.999713
9,500 10,000	0.903085 0.914199	$0.765338  0.653279 \times 10^{-5}$	0.105956 0.090442	100,000	0.999905



0.077600 0.066913 0.057970 0.050448 0.038689 0.030131 0.023794 0.019026 0.012574 0.008629 0.003828 0.001945 0.000656 0.000279 0.000058 0.000019



#### **Emission from Real Surfaces**



$$\varepsilon(T) = \frac{\int_0^\infty \varepsilon_{\lambda}(\lambda, T) E_{\lambda, b}(\lambda, T) d\lambda}{E_b(T)}$$

## **Absorption, Reflection and Transmission by Real Surfaces**



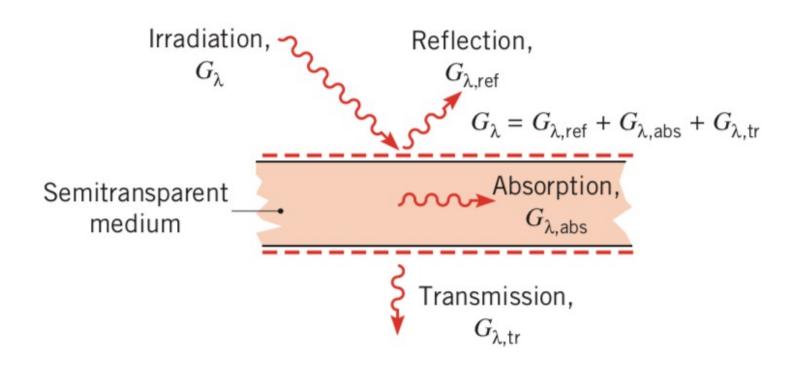


FIGURE 12.20 Spectral absorption, reflection, and transmission processes associated with a semitransparent medium.

## Absorption, Reflection and **Transmission by Real Surfaces**



#### TOTAL ABSORBTIVITY

$$\alpha = \frac{\int_0^\infty \alpha_{\lambda}(\lambda) G_{\lambda}(\lambda) d\lambda}{\int_0^\infty G_{\lambda}(\lambda) d\lambda}$$

#### TOTAL REFLECTIVITY

$$\alpha = \frac{\int_0^\infty \alpha_\lambda(\lambda) G_\lambda(\lambda) d\lambda}{\int_0^\infty G_\lambda(\lambda) d\lambda} \qquad \rho = \frac{\int_0^\infty \rho_\lambda(\lambda) G_\lambda(\lambda) d\lambda}{\int_0^\infty G_\lambda(\lambda) d\lambda}$$

#### TOTAL TRANSMISSIVITY

$$\tau = \frac{\int_0^\infty G_{\lambda, \text{tr}}(\lambda) \, d\lambda}{\int_0^\infty G_{\lambda}(\lambda) \, d\lambda} = \frac{\int_0^\infty \tau_{\lambda}(\lambda) G_{\lambda}(\lambda) \, d\lambda}{\int_0^\infty G_{\lambda}(\lambda) \, d\lambda}$$



#### Kirchhoff's Law

$$\varepsilon_{\lambda} = \alpha_{\lambda}$$

If surface is diffuse or if G is diffuse

$$\varepsilon = \alpha$$

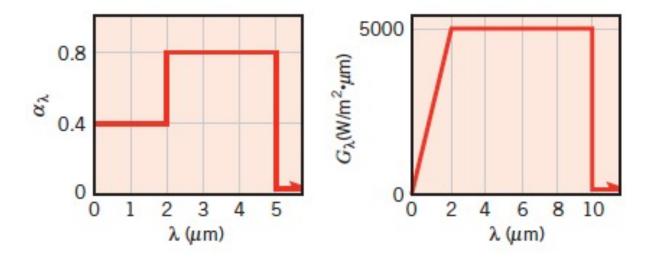
If the surface is grey

Grey surface Properties independent of wavelength



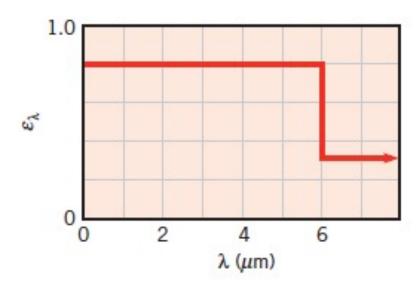
## **Example**

12.58 Consider an opaque, diffuse surface for which the spectral absorptivity and irradiation are as follows:



What is the total absorptivity of the surface for the prescribed irradiation? If the surface is at a temperature of 1250 K, what is its emissive power?

#### 12.59 The spectral emissivity of an opaque, diffuse surface is as shown.



- (a) If the surface is maintained at 1000 K, what is the total, hemispherical emissivity?
- (b) What is the total, hemispherical absorptivity of the surface when irradiated by large surroundings of emissivity 0.8 and temperature 1500 K?
- (c) What is the radiosity of the surface when it is maintained at 1000 K and subjected to the irradiation prescribed in part (b)?











## Thank You

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