## SIZE REDUCTION

- Large particles of solids are cut or broken into small pieces
in food-processing industry - eg. grind wheat to flour
in ore-processing \& cement industries - eg copper ores, nickel, cobalt ores $\boldsymbol{\&}$ iron ores are ground before chemical processing
- reasons:

1. occurs in sizes that are too large to be used
2. so separation can be carried out
3. increases the reactivity
4. reduces bulk of materials for easier handling and for waste disposal

## SIZE REDUCTION

- methods:

1. Compression or crushing


- coarse reduction of hard solids to coarse sizes

2. Impact/hammer


- gives coarse, medium or fine sizes

3. Attrition or rubbing $\square$ - yields very fine products
4. Cutting


- give definite sizes, sometimes a definite shape


## SIZE REDUCTION



- An ideal crusher would:

1. have a large capacity
2. require a small power input per unit of product
3. yield a product of the single size distribution desired

- cost of power is a major expense in size reduction equipment, so the factors that control this cost are important


## EFFICIENCY

Crushing efficiency, $\eta_{C}$

$$
\eta_{C}=\frac{\text { surface energy created by crushing }}{\text { energy absorbed by the solid }}
$$

$$
\eta_{C}=\frac{e_{S}\left(A_{w b}-A_{w a}\right)}{W_{n}}
$$

$e_{S}=$ surface energy per unit area
$W_{n}=$ energy absorbed by a unit mass
$A_{w o} A_{w b}=$ areas per unit mass of feed and product
Mechanical efficiency, $\eta_{m}$

$$
\begin{aligned}
\eta_{m} & =\frac{\text { energy absorbed by the solid }}{\text { total energy input }} \\
\eta_{m} & =\frac{W_{n}}{W}=\frac{e_{S}\left(A_{w b}-A_{w a}\right)}{W_{n} \eta_{C}}
\end{aligned}
$$

where

$$
\mathbf{W}=\text { energy input }=\frac{e_{S}\left(A_{w b}-A_{w a}\right)}{\eta_{m} \eta_{C}}
$$

## POWER REQUIRMENT

Power requirement by the size reduction machine is
where

$$
\mathrm{P}=\mathrm{W} \dot{\mathrm{~m}}=\frac{6 \dot{\mathrm{~m}} e_{S}}{\eta_{C} \eta_{m} \rho_{p}}\left(\frac{1}{\Phi_{\mathrm{b}} \overline{\mathrm{D}}_{\mathrm{sb}}}-\frac{1}{\Phi_{\mathrm{a}} \overline{\mathrm{D}}_{\mathrm{sa}}}\right)
$$

$P=$ power required
$\dot{\mathrm{m}}=$ feed rate
$\mathbf{D}_{\mathrm{sa}}, \overline{\mathbf{D}}_{\mathrm{sb}}=$ volume-surface mean dia. of feed \& product, respectively
$\eta_{C}=$ crushing efficiency
$\eta_{m}=$ mechanical efficiency
$\rho_{\mathrm{p}}=$ density of particle
$\mathrm{e}_{\mathrm{S}}=$ surface energy per unit area
$\Phi_{\mathrm{a}}, \Phi_{\mathrm{b}}=$ sphericity of feed and product, respectively

$$
\frac{6}{D_{s}=\frac{6}{\Phi_{s} A_{w} \rho_{p}}}=\frac{1}{\sum_{i=1}^{N}\left(\frac{x_{i}}{\bar{D}_{p i}}\right)} \quad \text { and } \quad A_{w}=\frac{6}{\Phi_{s} \rho_{p}} \sum_{i=1}^{N} \frac{x_{i}}{-}
$$

## SIZE REDUCTION

Highly energy intensive- 5\% of all electricity generated used
Most inefficient unit operation in terms of energy
$\mathbf{9 9 \%}$ goes to heat and noise
$1 \%$ goes to creating new interfacial area
Finer sizes much more costly in term of energy
Equations to estimate energy due to :
Rittinger (1867)
Kick (1885)
Bond (1952)
Kick's law - better for larger particles
Rittinger's law - better for fine grinding


## POWER REQUIRED IN SIZE REDUCTION

## Rittinger's law :

work required in crushing is proportional to the new surface created
where

$$
\frac{P}{\dot{m}}=K_{r}\left(\frac{1}{D_{s b}}-\frac{1}{D_{s a}}\right)
$$

$P=$ power required
$K_{r}=$ Rittinger's coefficient

$$
\mathbf{K}_{\mathrm{r}}=\frac{\mathbf{6 e}_{\mathrm{s}}}{\eta_{c} \eta_{m} \rho_{p}}\left(\frac{1}{\Phi_{b}}-\frac{1}{\Phi_{a}}\right)
$$

m = feed rate
$\mathbf{D}_{\mathrm{sa}}, \mathbf{D}_{\mathrm{sb}}=$ volume-surface mean dia. of feed $\boldsymbol{\&}$ product, respectively
$\eta_{C}=$ crushing efficiency
$\eta_{m}=$ ratio of energy absorbed to energy input
$\rho_{\mathrm{p}}=$ density of particle
$\mathrm{e}_{\mathrm{S}}=$ surface energy per unit area
$\Phi_{\mathrm{a}}, \Phi_{\mathrm{b}}=$ sphericity of feed and product, respectively

## Example 1

A certain crusher accepts a feed rock having a volume-surface mean diameter of 2 cm and discharges a product of volume-surface mean diameter of 0.5 cm . The power required to crush 10 ton $/ \mathrm{h}$ is 8 HP . What should be the power consumption if the capacity is increased to 12 ton/h and the volume-surface mean diameter is reduced to 0.4 cm ? Use Rittinger's law.

$$
\frac{\mathbf{P}}{\dot{\mathrm{m}}}=K_{\mathrm{r}}\left(\frac{1}{\mathbf{D}_{\mathrm{sb}}}-\frac{1}{D_{\mathrm{sa}}}\right)
$$

## Example 2

A crusher was used to crush a material with a feed size of $\mathbf{- 5 . 0 8} \mathbf{c m}+3.81 \mathrm{~cm}$ and the power required was $3.73 \mathrm{KW} / t o n$. The screen analysis of the product was as follows: What would be the power required to crush 1 ton/h of the same material from a feed of $-4.44 \mathrm{~cm}+3.81 \mathrm{~cm}$ to a product of average product size $\mathbf{0 . 0 5 1}$ cm? Use Rittinger's law.

| Size of aperture (cm) | \% product |
| :---: | :---: |
| 0.63 | - |
| 0.38 | 26 |
| 0.203 | 18 |
| 0.076 | 23 |
| 0.051 | 8 |
| 0.025 | 17 |
| 0.013 | 8 |

$$
\frac{\mathbf{P}}{\dot{\mathbf{m}}}=\mathbf{K}_{\mathrm{r}}\left(\frac{\mathbf{1}}{\mathbf{D}_{\mathrm{sb}}}-\frac{\mathbf{1}}{\mathbf{D}_{\mathrm{sa}}}\right)
$$

## POWER REQUIRED IN SIZE REDUCTION

## Kick's Law :

Energy required to reduce a material in size was directly proportional to the size-reduction ratio

$$
\frac{P}{\dot{m}}=K_{k} \ln \frac{D_{s a}}{D_{s b}}
$$

where
$P=$ power required
$K_{k}$ is the Kick's coefficient
$\dot{\mathrm{m}}=$ feed rate
$D_{s a}, D_{s b}=$ volume-surface mean dia. of feed $\&$ product, respectively

## CRUSHING EFFICIENCY

## Bond's Law :

work required using a large-size feed is proportional to the square root of the surface/volume ratio of the product
where

$$
\frac{\mathrm{P}}{\dot{\mathrm{~m}}}=K_{\mathrm{b}}\left(\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pb}}}}-\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pa}}}}\right)
$$

$$
P=\text { power required }
$$

$$
\mathrm{K}_{\mathrm{b}}=\text { constant }
$$

$$
\dot{m}=\text { feed rate }
$$

If $\mathbf{8 0 \%}$ of the feed passes a mesh size of $D_{p a} \mathbf{m m}$ and $80 \%$ of the product passes a mesh size of $D_{p b} \mathbf{m m}$,
where

$$
\frac{\mathrm{P}}{\dot{\mathrm{~m}}}=0.3162 \mathrm{~W}_{\mathrm{i}}\left(\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pb}}}}-\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pa}}}}\right)
$$

$\mathrm{W}_{\mathrm{i}}=$ work index
$\mathrm{D}_{\mathrm{p} 9}, \mathrm{D}_{\mathrm{pb}}=$ dia. of feed \& product, respectively (mm)

## WORK INDEX

Gross energy ( $\mathbf{k W} / \mathrm{h}$ ) required per ton of feed needed to reduce a very large feed $\left(\bar{D}_{p i}=\infty\right)$ to such a size that $\mathbf{8 0 \%}$ of the product passes a $100 \mu \mathrm{~m}$ screen.

Include friction in the crusher \& power

| Material | Specific gravity | Work Index, $\mathbf{W}_{\mathbf{i}}$ |
| :--- | :---: | :---: |
| Bauxite | 2.20 | 8.78 |
| Cement clinker | 3.15 | 13.45 |
| Cement raw material | 2.67 | 10.51 |
| Clay | 2.51 | 6.30 |
| Coal | 1.4 | 13.00 |
| Coke | 1.31 | 15.13 |
| Granite | 2.66 | 15.13 |
| Gravel | 2.66 | 16.06 |
| Gypsum rock | 2.69 | 6.73 |
| Iron ore (hematite) | 3.53 | 12.84 |
| Limestone | 2.66 | 12.74 |
| Phosphate rock | 2.74 | 9.92 |
| Quartz | 2.65 | 13.57 |
| Shale | 2.63 | 15.87 |
| Slate | 2.57 | 14.30 |
| Trap rock | 2.87 | 19.32 |

## Example 3

1. What is the power required to crush $100 \mathrm{ton} / \mathrm{h}$ of limestone if $80 \%$ of the feed pass a 2 -in screen and $80 \%$ of the product a $1 / 8$ in screen?

## Solution:

The work index for limestone is 12.74 .

$$
\frac{\mathrm{P}}{\dot{\mathrm{~m}}}=0.3162 \mathrm{~W}_{\mathrm{i}}\left(\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pb}}}}-\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pa}}}}\right)
$$

$$
\begin{aligned}
& \dot{\mathrm{m}}=100 \mathrm{ton} / \mathrm{h} \\
& D_{p a}=2 * 25.4=50.8 \mathrm{~mm} \\
& D_{p b}=0.125 * 25.4=3.175 \mathrm{~mm}
\end{aligned}
$$

The power required is :

$$
\begin{aligned}
& P=100 * 0.3162 * 12.74\left(\frac{1}{\sqrt{3.175}}-\frac{1}{\sqrt{50.8}}\right) \\
& =169.6 k \mathrm{~W}
\end{aligned}
$$

## Example 3

2. $\mathbf{8 0 \%}$ of feed (ore) is less than 5.08 cm in size and the product size is such that $80 \%$ is less than 0.685 cm . The power required is 89.5 kW . What will be the power required using the same feed so that $80 \%$ is less than 0.3175 cm?

$$
\frac{\mathrm{P}}{\dot{\mathrm{~m}}}=0.3162 \mathrm{~W}_{\mathrm{i}}\left(\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pb}}}}-\frac{1}{\sqrt{\mathrm{D}_{\mathrm{pa}}}}\right)
$$

## Solution Example 3-Q2

- $\mathrm{P}_{1}=89.5 \mathrm{~kW}$
- $W_{i}=19.32$
- $D_{\text {pa1 }}=50.8 \mathrm{~mm}$
- $\mathrm{D}_{\mathrm{pb} 1}=6.35 \mathrm{~mm}$
- $\mathrm{m}_{\text {flowrate }}=$ ?
- $\mathrm{D}_{\mathrm{pb} 2}=3.18 \mathrm{~mm}$
- $\mathrm{P}_{2}=$ ?


## Example 4

Granite rock is crushed with a uniform feed of 2 in-spheres. The screen analysis is given in the table below. The power required to crush this material is 500 kW ; of this 20 kW is needed to operate the empty mill. The feed rate is at $150 \mathrm{ton} / \mathrm{hr}$. Calculate the power required for the second operation using:

| a) Rittinger's Law <br> b) Kick's law | Mesh | $\mathrm{x}_{1}(\%)$ | $\mathrm{x}_{2}(\%)$ |
| :---: | :---: | :---: | :---: |
|  | 3/4 | 2.1 | - |
|  | 4/6 | 12.4 | 4.1 |
|  | 6/8 | 15.2 | 9.6 |
|  | 8/10 | 17.6 | 10.1 |
|  | 10/12 | 14.8 | 13.4 |
|  | 12/14 | 13.1 | 15.7 |
|  | 14/20 | 10.8 | 18.3 |
|  | 20/28 | 8.3 | 13.2 |
|  | 28/35 | 5.2 | 9.6 |
| Change 50 to 150 | 35/48 | 0.5 | 3.0 |
|  | 48/65 | - | 1.8 |
|  | 65/100 | - | 0.9 |
| $\searrow$ | 100/150 | - | 0.3 |

## Example 5

Trap rock is crushed in a gyratory crusher. The feed is nearly uniform 2-in. spheres. The differential screen analysis of the product is given in column (1) of Table 1 below The power required to crush this material is 400 kW . Of this 10 kW is needed to operate the empty mill. By reducing the clearance between the crushing head and the cone, the differential screen analysis of the product becomes that given in column (2) in Table1 below. From (a) Rittinger's law and (b) Kick's law, calculate the power required for the second operation. The feed rate is 110 ton $/ \mathrm{h}$.

| Tyler Mesh size | Mesh size in <br> $\mu \mathrm{m}$ | First grind <br> product (\%) | Second grind <br> product (\%) |
| :--- | :--- | :--- | :--- |
| $-4+6$ | 4699 to 3327 | 3.1 | - |
| $-6+8$ | 3327 to | 10.3 | 3.3 |
| $-8+10$ | 2362 to | 20.0 | 8.2 |
| $-10+14$ | 1651 to | 18.6 | 11.2 |
| $-14+20$ | 1168 to | 15.2 | 12.3 |
| $-20+28$ | 833 to | 12.0 | 13.0 |
| $-28+35$ | 589 to | 9.5 | 19.5 |
| $-35+48$ | 417 to | 6.5 | 13.5 |
| $-48+65$ | 295 to | 4.3 | 8.5 |
| -65 |  | 0.5 | - |
| $-65+100$ | 208 to | - | 6.2 |
| $-100+150$ | 147 to | - | 4.2 |
| -150 | 104 | - | 0.3 |

## Solution

| Mesh | Product 1 | Dpi $_{\mathrm{av}}$ | xi1 | xi1/Dpi av |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $4 / 6$ | 3.1 | 4.013 | 0.031 | 0.007725 |  |  |  |  |
| $6 / 8$ | 10.3 | 2.845 | 0.103 | 0.036204 |  |  |  |  |
| $8 / 10$ | 20 | 2.007 | 0.2 | 0.099651 |  |  |  |  |
| $10 / 14$ | 18.6 | 1.409 | 0.186 | 0.132009 |  |  |  |  |
| $14 / 20$ | 15.2 | 1.001 | 0.152 | 0.151848 |  |  |  |  |
| $20 / 28$ | 12 | 0.711 | 0.12 | 0.168776 |  |  |  |  |
| $28 / 35$ | 9.5 | 0.503 | 0.095 | 0.188867 |  |  |  |  |
| $35 / 48$ | 6.5 | 0.356 | 0.065 | 0.182584 |  |  |  |  |
| $48 / 65$ | 4.3 | 0.252 | 0.043 | 0.170635 |  |  |  |  |
| 65 | 0.5 | 0.178 | 0.005 | 0.02809 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | Exi1/Dpi ${ }_{\mathrm{av}}$ |
|  | total |  |  | 1.166389 |  |  |  |  |


| Mesh | Product 2 | Xi2 | Dpiav | $x i 2 / D p_{\text {av }}$ |
| :---: | :---: | :---: | :---: | :---: |
| 6/8 | 3.3 | 0.033 | 2.845 | 0.011599 |
| 8/10 | 8.2 | 0.082 | 2.007 | 0.040857 |
| 10/14 | 11.2 | 0.112 | 1.409 | 0.079489 |
| 14/20 | 12.3 | 0.123 | 1.001 | 0.122877 |
| 20/28 | 13 | 0.13 | 0.711 | 0.182841 |
| 28/35 | 19.5 | 0.195 | 0.503 | 0.387674 |
| 35/48 | 13.5 | 0.135 | 0.356 | 0.379213 |
| 48/65 | 8.5 | 0.085 | 0.252 | 0.337302 |
| 65/100 | 6.2 | 0.062 | 0.178 | 0.348315 |
| 100/150 | 4 | 0.04 | 0.126 | 0.31746 |
| 150 | 0.3 | 0.003 | 0.089 | 0.033708 |
|  | total |  |  |  |
|  | 100 |  |  | 2.241335 |

Size Reduction
Slide18

- Rittinger's Law Kick's Law

$$
\frac{P}{\dot{m}}=K_{r}\left(\frac{1}{\bar{D}_{s b}}-\frac{1}{\bar{D}_{s a}}\right) \quad \frac{P}{\dot{m}}=K_{k} \ln \frac{\bar{D}_{s a}}{\bar{D}_{s b}}
$$

- $\mathrm{Dsb}_{\mathrm{ave}}=1 / 1.166389($ produk 1$)=0.857347 \mathrm{~mm}$
- Dsa $_{\text {ave }}=2 \mathrm{inci}=50.8 \mathrm{~mm}$
- $P=390 \mathrm{~kW} /$ ton
- $\mathrm{m}_{\text {flow rate }}=110$ ton $/ \mathrm{hr}$
- $K_{r}=3.039$
- $\mathrm{Dsb}_{\text {ave }}=1 / 2.241335($ produk 2$)=0.446163$ mm
- $\mathrm{Dsa}_{\mathrm{ave}}=2 \mathrm{inci}=50.8 \mathrm{~mm}$
- $\mathrm{m}_{\text {flow rate }}=110$ ton $/ \mathrm{hr}$
- $K_{r}=3.039$
- $P=751 \mathrm{~kW}$
- Total Power required =

$$
751 \mathrm{~kW}+10 \mathrm{~kW}=761 \mathrm{~kW}
$$

## SIZE REDUCTION EQUIPMENTS

selection of equipments:

1) input size
2) product size
3) hardness
4) brittleness
5) plasticity
6) flammability
major types:
crushers, ultrafine grinders, grinders $\boldsymbol{\&}$ cutting machines

## CRUSHERS

- Slow-speed machine for coarse reduction of large quantities of solids
- break large pieces of solid material into small lumps

Primary crusher - accepts anything from mine \& breaks into $\mathbf{1 5 0 - 2 5 0} \mathbf{~ m m}$
Secondary crusher - reduces lumps into 6 mm main types:

1) Jaw crushers
2) Gyratory crushers
3) smooth-roll crushers
4) toothed-roll crushers


Gyratory crusher

## GRINDERS

- for intermediate duty (from crushers to grinders for further reduction)
- reduce crushed feed to powder
- product from intermediate grinder might pass a 40-mesh screen
- product from fine grinder would pass a $\mathbf{2 0 0}$-mesh screen ( $\mathbf{7 4} \mu \mathrm{m}$ screen) commercial grinders:

1) Hammer mills \& impactor
2) rolling-compression machines
3) Attrition mills
4) Tumbling mills


Spin mill

hammer

## SIZE REDUCTION EQUIPMENTS

[incrushers (coarse and fine)

- Jaw crushers
- Gyratory crushers
- Crushing rolls

TGrinders (intermediate and fine)

- Hammer mills; impactors
- Rolling-compression mills
- Attrition mills
- Tumbling mills

TUltrafine grinders

- hammer mills with internal classification
- Fluid-energy mills
- Agitated mills

Cutting machines

- Knife cutters; dicers; slitters


## CRUSHER



Blake jaw crusher


Gyratory Crusher

## GRINDERS



Impactor


Roller mill

## CUTTER



Rotary knife cutter

## SIZE REDUCTION EQUIPMENTS



Ball mill in Mining Industry


In Cement Industry

